

The following excerpt are pages from the North American Product Technical Guide, Volume 2: Anchor Fastening, Edition 21.

Please refer to the publication in its entirety for complete details on this product including data development, product specifications, general suitability, installation, corrosion and spacing and edge distance guidelines. US&CA: <u>https://submittals.us.hilti.com/PTGVol2/</u>

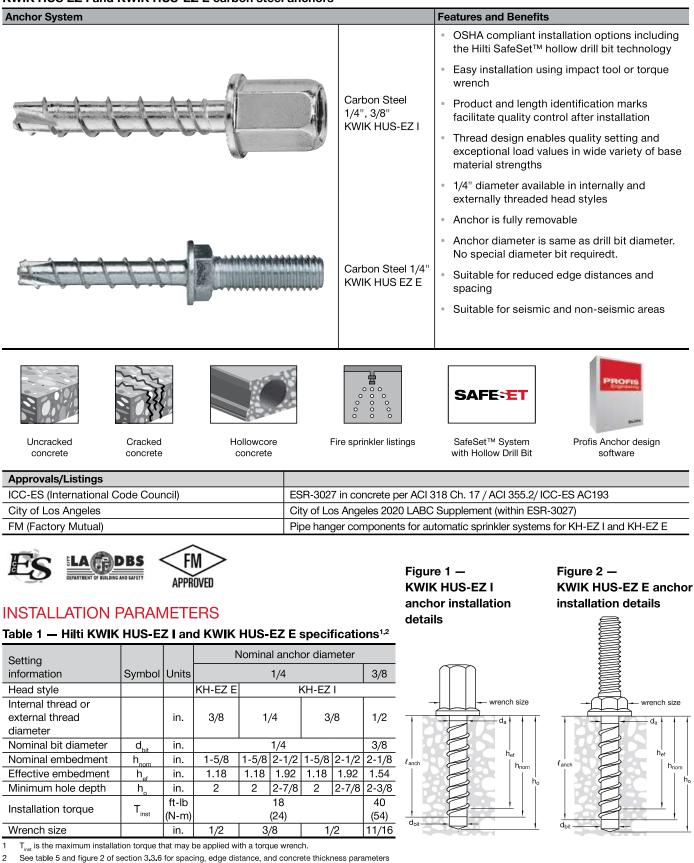
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1-800-879-8000 www.hilti.com

3.3.8 KWIK HUS-EZ I AND KWIK HUS-EZ E CARBON STEEL SCREW ANCHOR

PRODUCT DESCRIPTION

KWIK HUS EZ I and KWIK HUS-EZ E carbon steel anchors



366 Anchor Fastening Technical Guide Edition 21 | 3.0 ANCHORING SYSTEMS | 3.3.8 KWIK HUS-EZ | AND KWIK HUS-EZ E CARBON STEEL SCREW ANCHOR Hilti, Inc. 1-800-879-8000 | en español 1-800-879-5000 | www.hilti.com | Hilti (Canada) Corporation | www.hilti.ca | 1-800-363-4458

DESIGN INFORMATION IN CONCRETE PER ACI 318

ACI 318 Chapter 17 design

The load values contained in this section are Hilti Simplified Design Tables. The load tables in this section were developed using the Strength Design parameters and variables of ESR-3027 and the equations within ACI 318 Chapter 17. For a detailed explanation of the Hilti Simplified Design Tables, refer to section 3.1.8. Data tables from ESR-3027 are not contained in this section, but can be found at www.icc-es.org or at www.hilti.com.

					Tension - φN	1				Shear	· - φV _n	
anchor diameter	embed.	(17.2 MPa)	f' _c = 3,000 psi (20.7 MPa) lb (kN)	f' _c = 4,000 psi (27.6 MPa) lb (kN)	f' _c = 5,000 psi (34.5 MPa) Ib (kN)	f' _c = 6,000 psi (41.4 MPa) lb (kN)	f' _c = 7,000 psi (48.3 MPa) Ib (kN)	f' _c = 8,000 psi (55.2 MPa) Ib (kN)	f' _c = 2,500 psi (17.2 MPa) lb (kN)	f' _c = 3,000 psi (20.7 MPa) lb (kN)	f' _c = 4,000 psi (27.6 MPa) lb (kN)	f' _c = 6,000 psi (41.4 MPa) Ib (kN)
	1-5/8	585	620	675	725	765	800	830	1,075	1,180	1,360	1,670
1/4	(41)	(2.6)	(2.8)	(3.0)	(3.2)	(3.4)	(3.6)	(3.7)	(4.8)	(5.2)	(6.0)	(7.4)
1/4	2-1/2	1,525	1,670	1,930	2,160	2,365	2,555	2,730	2,235	2,450	2,825	3,460
	(64)	(6.8)	(7.4)	(8.6)	(9.6)	(10.5)	(11.4)	(12.1)	(9.9)	(10.9)	(12.6)	(15.4)
2 /0	2-1/8	1,490	1,635	1,885	2,110	2,310	2,495	2,665	1,605	1,760	2,030	2,485
3/8	(54)	(6.6)	(7.3)	(8.4)	(9.4)	(10.3)	(11.1)	(11.9)	(7.1)	(7.8)	(9.0)	(11.1)

Table 2 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E design strength with concrete / pullout failure in uncracked concrete^{1,2,3,4}

Table 3 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E design strength with concrete/pullout failure in cracked concrete^{1,2,3,4,5}

				-	Tension - φN _,	ı				Shear	- φV _n	
	embed.	f' _c = 2,500 psi (17.2 MPa)	f' _c = 3,000 psi (20.7 MPa)	f' _c = 4,000 psi (27.6 MPa)	f' _c = 5,000 psi (34.5 MPa)	f' _c = 6,000 psi (41.4 MPa)	f' _c = 7,000 psi (48.3 MPa)	f' _c = 8,000 psi (55.2 MPa)	f' _c = 2,500 psi (17.2 MPa)	f' _c = 3,000 psi (20.7 MPa)	f' _c = 4,000 psi (27.6 MPa)	f' _c = 6,000 psi (41.4 MPa)
in.	in. (mm)	lb (kN)										
	1-5/8	300	315	345	370	390	410	425	765	835	965	1,180
1/4	(41)	(1.3)	(1.4)	(1.5)	(1.6)	(1.7)	(1.8)	(1.9)	(3.4)	(3.7)	(4.3)	(5.2)
1/4	2-1/2	760	830	960	1,070	1,175	1,270	1,355	1,585	1,735	2,000	2,450
	(64)	(3.4)	(3.7)	(4.3)	(4.8)	(5.2)	(5.6)	(6.0)	(7.1)	(7.7)	(8.9)	(10.9)
3/8	2-1/8	1,055	1,155	1,335	1,495	1,635	1,765	1,890	1,135	1,245	1,440	1,760
3/8	(54)	(4.7)	(5.1)	(5.9)	(6.7)	(7.3)	(7.9)	(8.4)	(5.0)	(5.5)	(6.4)	(7.8)

1 See section 3.1.8 to convert design strength value to ASD value.

2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

Apply spacing, edge distance, and concrete thickness factors in tables 5 and 6 as necessary. Compare to the steel values in table 4. 3

The lesser of the values is to be used for the design.

Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ_a as follows:

for sand-lightweight, $\lambda_a = 0.68$; for all-lightweight, $\lambda_a = 0.60$

Tabular values are for static loads only. For seismic tension loads, multiply cracked concrete tabular values in tension by the following reduction factors: 1/4-in diameter by 1-5/8-in nominal embedment depth - $\alpha_{N,seis} = 0.60$

1/4-in diameter by 2-1/2-in nominal embedment depth $-\alpha_{N,aeie} = 0.75$ 3/8-in diameter by 2-1/8-in nominal embedment depth $-\alpha_{N,aeie} = 0.75$

No reduction needed for seismic shear. See Section 3.1.8 for additional information on seismic applications.

Table 4 — Steel design strength for Hilti KWIK HUS-EZ I and KWIK HUS-EZ E anchors^{1,2}

Nominal anchor diameter in.	Nominal internal thread diameter in.	Tensile³	Shear⁴ φV _{sa} Ib (kN)	Seismic shear ⁵ φV _{sa} Ib (kN)
	1/4-20	3,680	815	365
1/4	UNC	(16.4)	(3.6)	(1.6)
1/4	3/8-16	3,680	790	670
	UNC	(16.4)	(3.5)	(3.0)
3/8	1/2-13	5,990	1,130	1,130
5/0	UNC	(26.6)	(5.0)	(5.0)

1 See section 3.1.8 to convert design strength value to ASD value.

2 Hilti KWIK HUS-EZ I anchors are to be considered brittle steel elements.

3 Tension $\phi N_{sa} = \phi A_{se,N} f_{uta}$ as noted in ACI 318 Chapter 17.

Seismic shear values determined by seismic shear tests with ϕ V_{es} $\leq \phi$ 0.60 A_{eav} f_{eta} as noted in ACI 318 Chapter 17. 5

See Section 3.1.8 for additional information on seismic applications.

⁴ Shear determined by static tests with $\phi V_{sa} < \phi 0.60 A_{se,V} f_{uta}$ as noted in ACI 318 Chapter 17.



									E	dge distar	nce in shea	ar		
1,	/4-in. KH-	EZ	Spacine in ter	0		istance tension		g factor near³	⊥ towa	rd edge	ll to an from	d away edge		nickness n shear⁴
uncr	acked cor	ncrete	f_{j}	AN	f_{1}	RN	f_{j}	AV	f f	RV	f_{1}	RV	f f	HV
Embe	edment	in.	1-5/8	2-1/2	1-5/8	2-1/2	1-5/8	2-1/2	1-5/8	2-1/2	1-5/8	2-1/2	1-5/8	2-1/2
h	nom	(mm)	(41)	(64)	(41)	(64)	(41)	(64)	(41)	(64)	(41)	(64)	(41)	(64)
	1-1/2	(38)	0.71	0.63	0.78	0.65	0.59	0.56	0.40	0.21	0.78	0.42	n/a	n/a
a)	2	(51)	0.78	0.67	1.00	0.77	0.62	0.58	0.61	0.33	1.00	0.65	n/a	n/a
concrete	2-1/2	(64)	0.85	0.72		0.90	0.65	0.60	0.86	0.46		0.90	n/a	n/a
lCr	3	(76)	0.92	0.76		1.00	0.68	0.62	1.00	0.60		1.00	n/a	n/a
00	3-1/4	(83)	0.96	0.78			0.70	0.63		0.68			0.88	n/a
$\gtrsim \widehat{E}$	3-1/2	(89)	0.99	0.80			0.71	0.64		0.76			0.92	n/a
distance (c _a) / s (h) - in. (mm)	4	(102)	1.00	0.85			0.74	0.66		0.92			0.98	n/a
in (4-1/8	(105)		0.86			0.75	0.66		0.97			1.00	0.81
- i	4-1/2	(114)		0.89			0.77	0.68		1.00				0.84
list (h)	5	(127)		0.93			0.80	0.70						0.89
s) / edge dist thickness (h)	5-1/2	(140)		0.98			0.83	0.72						0.93
edge kness	6	(152)		1.00			0.86	0.74						0.97
ic ∕ ⊕	7	(178)					0.92	0.78						1.00
th (s)	8	(203)					0.98	0.82						
bu	9	(229)					1.00	0.86						
aci	10	(254)						0.89						
Spacing (s) th	11	(279)						0.93						
•,	12	(305)						0.97						
	14	(356)						1.00						

Table 5 — Load adjustment factors for 1/4-in. diameter Hilti KWIK HUS-EZ I and KWIK HUS-EZ E in uncracked concrete^{1,2}

Table 6 — Load adjustment factors for 1/4-in. diameter Hilti KWIK HUS-EZ I and KWIK HUS-EZ E in cracked concrete^{1,2}

									E	dge distar	nce in shea	ar		
			Spacin	g factor	Edge d	istance	Spacin	g factor			II to an	d away	Conc. tł	nickness
1	/4-in. KH-	EZ	in ter	nsion	factor in	tension	in sł	near ³	⊥ towa	rd edge	from	edge	factor i	n shear ⁴
cra	cked cond	crete	f	AN	f	RN	f	AV	f f	RV	f	RV	f f	HV
Embe	edment	in.	1-5/8	2-1/2	1-5/8	2-1/2	1-5/8	2-1/2	1-5/8	2-1/2	1-5/8	2-1/2	1-5/8	2-1/2
		(mm)	(41)	(64)	(41)	(64)	(41)	(64)	(41)	(64)	(41)	(64)	(41)	(64)
•	nom	. ,	. ,	. ,	0.88	. ,	0.59	. ,	0.40	()	0.80	0.43		
	1-1/2	(38)	0.71	0.63		0.65		0.56		0.21			n/a	n/a
	2	(51)	0.78	0.67	1.00	0.77	0.62	0.58	0.62	0.33	1.00	0.66	n/a	n/a
te	2-1/2	(64)	0.85	0.72		0.90	0.65	0.60	0.87	0.46		0.90	n/a	n/a
Spacing (s) / edge distance (c_a) / concrete thickness (h) - in. (mm)	3	(76)	0.92	0.76		1.00	0.68	0.62	1.00	0.60		1.00	n/a	n/a
Ű	3-1/4	(83)	0.96	0.78			0.70	0.63		0.68			0.89	n/a
~ _	3-1/2	(89)	0.99	0.80			0.71	0.64		0.76			0.92	n/a
mn (c_a)	4	(102)	1.00	0.85			0.74	0.66		0.93			0.98	n/a
- Ce	4-1/8	(105)		0.86			0.75	0.66		0.97			1.00	0.81
- ii	4-1/2	(114)		0.89			0.77	0.68		1.00				0.85
(L) dist	5	(127)		0.93			0.80	0.70						0.89
ge (5-1/2	(140)		0.98			0.83	0.72						0.93
kn ed	6	(152)		1.00			0.86	0.74						0.98
hic	7	(178)					0.92	0.78						1.00
g t	8	(203)					0.98	0.82						
ci.	9	(229)					1.00	0.86						
ba	10	(254)						0.90						
0)	11	(279)						0.94						
	12	(305)						0.98						
	14	(356)						1.00						

1 Linear interpolation not permitted.

2 When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Engineering software or perform anchor calculation using design equations from ACI 318 Chapter 17.

3 Spacing factor reduction in shear, f_{AV} assumes an influence of a nearby edge. If no edge exists, then $f_{AV} = f_{AN}$.

4 Concrete thickness reduction factor in shear, f_{HV} assumes an influence of a nearby edge. If no edge exists, then f_{HV} = 1.0.

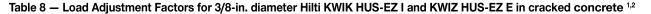
If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa).

Check with table 5 and figure 2 of section 3.3.6 to calculate permissable edge distance, spacing and concrete thickness combinations.

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																	Edge	e distar	nce in s	shear						
3	/8-in. K uncrac concr	ked		Spacin in tei f		r		actor in	istance I tensic			Spacing in sh		r	-	<i>c</i>	rd edg	e		from	d away edge ^{RV}	/	Cond	c. thick in sh f		actor
Em	bedme	nt in.	1-5/8	2-1/8	2-1/2	3-1/4	1-5/8	2-1/8		3-1/4	1-5/8	2-1/8	2-1/2	3-1/4	1-5/8	2-1/8	2-1/2	3-1/4	1-5/8	2-1/8	2-1/2	3-1/4	1-5/8	2-1/8	2-1/2	3-1/4
	h _{nom}	(mm)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)
	1-1/2	2 (38)	n/a	n/a	n/a	n/a	0.58	0.62	0.63	0.57	n/a	n/a	n/a	n/a	0.49	0.32	0.25	0.08	0.58	0.62	0.50	0.17	n/a	n/a	n/a	n/a
Ê	2	(51)	n/a	n/a	n/a	n/a	0.76	0.75	0.75	0.66	n/a	n/a	n/a	n/a	0.75	0.49	0.38	0.13	0.76	0.75	0.75	0.26	n/a	n/a	n/a	n/a
(mm)	2-1/-	1 (57)	0.84	0.74	0.70	0.65	0.86	0.82	0.81	0.70	0.65	0.62	0.60	0.55	0.90	0.59	0.46	0.16	0.90	0.82	0.81	0.31	n/a	n/a	n/a	n/a
.⊑	2-1/	2 (64)	0.88	0.77	0.72	0.67	0.95	0.91	0.88	0.75	0.67	0.63	0.61	0.55	1.00	0.69	0.54	0.18	1.00	0.91	0.88	0.37	n/a	n/a	n/a	n/a
- (4)	3	(76)	0.95	0.82	0.77	0.70	1.00	1.00	1.00	0.85	0.71	0.66	0.63	0.56		0.90	0.71	0.24		1.00	1.00	0.48	n/a	n/a	n/a	n/a
	3-1/-	4 (83)	0.99	0.85	0.79	0.72				0.90	0.72	0.67	0.64	0.57		1.00	0.80	0.27				0.54	0.95	n/a	n/a	n/a
thickness	3-1/	2 (89)	1.00	0.88	0.81	0.73				0.95	0.74	0.68	0.65	0.58			0.89	0.30				0.61	0.98	n/a	n/a	n/a
j	4	(102)		0.93	0.86	0.77				1.00	0.78	0.71	0.68	0.59			1.00	0.37				0.74	1.00	0.91	0.84	n/a
e th	4-1/	· · · · /		0.99	0.90	0.80					0.81	0.73	0.70	0.60				0.44				0.88			0.89	n/a
ret	4-3/-	· · ·		1.00	0.93	0.82					0.83	0.75	0.71	0.60				0.48				0.96			0.91	0.639
ouc	5	(127)			0.95	0.83					0.84	0.76	0.72	0.61				0.52				1.00			0.94	0.655
(c_)/concrete	6	(152)			1.00	0.90					0.91	0.81	0.76	0.63				0.68							1.00	0.718
		(178)				0.97					0.98	0.86	0.81	0.65				0.86								0.775
distance	8	(203)				1.00					1.00	0.91	0.85	0.67				1.00								0.829
sta	9	(229)										0.97	0.90	0.69												0.879
	10	(254)										1.00	0.94 0.98	0.71 0.74												0.927
dg	11	(279) (305)											1.00	0.74												1.000
(s)/edge	14	(305)											1.00	0.76												1.000
		(406)												0.80												<u> </u>
pacing	18	(400)												0.84												<u> </u>
Spe	20	(508)												0.93												<u> </u>
	24	(610)												1.000												

Table 7 — Load Adjustment Factors for 3/8-in. diameter KWIK HUS-EZ I and KWIK HUS-EZ E in uncracked concrete ^{1,2}



																Edge	e distar	nce in s	hear						
n. KH- acked ncrete		\$	in ter	nsion	r		actor in	tensio		9	in sh	iear ³	r	L		•	e		from	edge	,	Cond	in sh	iear ⁴	actor
ment	in.	1-5/8	2-1/8	2-1/2	3-1/4	1-5/8	2-1/8	2-1/2	3-1/4	1-5/8	2-1/8	2-1/2	3-1/4	1-5/8	2-1/8	2-1/2	3-1/4	1-5/8	2-1/8	2-1/2	3-1/4	1-5/8	2-1/8	2-1/2	3-1/4
n	(mm)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)	(41)	(54)	(64)	(83)
1-1/2	(38)	n/a	n/a	n/a	n/a	0.92	0.74	0.66	0.57	n/a	n/a	n/a	n/a	0.49	0.32	0.25	0.09	0.92	0.64	0.50	0.17	n/a	n/a	n/a	n/a
2	(51)	n/a	n/a	n/a	n/a	1.00	0.90	0.79	0.66	n/a	n/a	n/a	n/a	0.76	0.50	0.39	0.13	1.00	0.90	0.77	0.26	n/a	n/a	n/a	n/a
2-1/4	(57)	0.84	0.74	0.70	0.65	1.00	0.98	0.85	0.70	0.66	0.62	0.60	0.55	0.90	0.59	0.46	0.16	1.00	0.98	0.85	0.31	n/a	n/a	n/a	n/a
2-1/2	(64)	0.88	0.77	0.72	0.67	1.00	1.00	0.92	0.75	0.67	0.63	0.61	0.55	1.00	0.69	0.54	0.18	1.00	1.00	0.92	0.37	n/a	n/a	n/a	n/a
3	(76)	0.95	0.82	0.77	0.70	1.00		1.00	0.85	0.71	0.66	0.63	0.56	1.00	0.91	0.71	0.24	1.00	1.00	1.00	0.48	n/a	n/a	n/a	n/a
3-1/4	· /														1.00	0.80					0.55		n/a	n/a	n/a
3-1/2	· /	1.00														0.90					0.61		n/a	n/a	n/a
4	<u>`</u>				-				1.00		-					1.00						1.00			n/a
,	· /																								n/a
4-3/4	· /		1.00																				1.00		0.64
5	· /											-									1.00				0.66
6	(/			1.00																				1.00	0.72
7	· /																								0.78
8	· /				1.00					1.00							1.00								0.83
9	· /																								0.88
	· /										1.00														0.93
	<u> </u>																								0.97
	· /											1.00													1.00
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	acked ncrete ment 1-1/2 2 2-1/4 2-1/2 3 3-1/4 3-1/2 4 4-1/2 4-3/4	norete nent in. 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1 Linear interpolation not permitted.

2 When combining multiple load adjustment factors (e.g. for a 4 anchor pattern in a corner with thin concrete member) the design can become very conservative. To optimize the design, use Hilti PROFIS Engineering software or perform anchor calculation using design equations from ACI 318 Chapter 17.

3 Spacing factor reduction in shear, f_{AV} assumes an influence of a nearby edge. If no edge exists, then $f_{AV} = f_{AN}$.

4 Concrete thickness reduction factor in shear, f_{HV} assumes an influence of a nearby edge. If no edge exists, then f_{HV} = 1.0.

If a reduction factor value is in a shaded cell, this indicates that this specific edge distance may not be permitted with a certain spacing (or vice versa).

Check table 5 and figure 2 of this section to calculate permissable edge distance, spacing and concrete thickness combinations.

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3.3.6



				Installation i	n lower flute			Installation in	n upper flute	
Nominal	Nominal internal	Nominal	Tensio	n - φN _n	Shear	- φV _n	Tensior	η - φΝ _n	Shear	- φV _n
anchor	thread diameter in.	embed.	f'	f' _c = 4,000 psi (27.6 MPa) Ib (kN)	f' = 3,000 psi (20.7 MPa) Ib (kN)	f' _c = 4,000 psi (27.6 MPa) Ib (kN)	f' = 3,000 psi (20.7 MPa) Ib (kN)	f' _c = 4,000 psi (27.6 MPa) Ib (kN)	f' _c = 3,000 psi (20.7 MPa) Ib (kN)	f' = 4,000 psi (27.6 MPa) Ib (kN)
		1-5/8	545	595	515	515	670	730	610	610
	1/4-20	(41)	(2.4)	(2.6)	(2.3)	(2.3)	(3.0)	(3.2)	(2.7)	(2.7)
	UNC	2-1/2	1,220	1,410	515	515	1,275	1,470	610	610
1 /4		(64)	(5.4)	(6.3)	(2.3)	(2.3)	(5.7)	(6.5)	(2.7)	(2.7)
1/4		1-5/8	545	595	615	615	670	730	915	915
	3/8-16	(41)	(2.4)	(2.6)	(2.7)	(2.7)	(3.0)	(3.2)	(4.1)	(4.1)
	UNC	2-1/2	1,220	1,410	615	615	1,275	1,470	915	915
		(64)	(5.4)	(6.3)	(2.7)	(2.7)	(5.7)	(6.5)	(4.1)	(4.1)
2/0	1/2-13	2-1/8	1,120	1,295	1,430	1,430	1,730	2,000	2,190	2,190
3/8	UNC	(54)	(5.0)	(5.8)	(6.4)	(6.4)	(7.7)	(8.9)	(9.7)	(9.7)

Table 9 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E in the soffit of uncracked lightweight concrete over metal deck^{1,2,3,4,5,6}

Table 10 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E in the soffit of cracked lightweight concrete over metal deck^{1,2,3,4,5,6,7,8}

				Installation i	n lower flute			Installation i	n upper flute	
Nominal	Nominal internal	Nominal	Tensio	n - φN _n	Shear	- φV _n	Tensior	η - φΝ _n	Shear	- φV _n
anchor	thread diameter in.	embed.		f' _c = 4,000 psi (27.6 MPa) Ib (kN)	f' _c = 3,000 psi (20.7 MPa) Ib (kN)	f'	f'	f'	f' _c = 3,000 psi (20.7 MPa) Ib (kN)	f' _c = 4,000 psi (27.6 MPa) Ib (kN)
		1-5/8	280	305	515	515	330	360	610	610
	1/4-20	(41)	(1.2)	(1.4)	(2.3)	(2.3)	(1.5)	(1.6)	(2.7)	(2.7)
	UNC	2-1/2	605	700	515	515	635	735	610	610
1 /4		(64)	(2.7)	(3.1)	(2.3)	(2.3)	(2.8)	(3.3)	(2.7)	(2.7)
1/4		1-5/8	280	325	615	615	330	380	915	915
	3/8-16	(41)	(1.2)	(1.4)	(2.7)	(2.7)	(1.5)	(1.7)	(4.1)	(4.1)
	UNC	2-1/2	605	700	615	615	635	735	915	915
		(64)	(2.7)	(3.1)	(2.7)	(2.7)	(2.8)	(3.3)	(4.1)	(4.1)
2 /0	1/2-13	2-1/8	795	920	1,430	1,430	1,225	1,415	2,190	2,190
3/8	UNC	(54)	(3.5)	(4.1)	(6.4)	(6.4)	(5.4)	(6.3)	(9.7)	(9.7)

See Section 3.1.8 to convert design strength value to ASD value. 1

2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

3 Tabular value is for one anchor per flute. Minimum spacing along the length of the flute is 3 x h_{nom} (nominal embedment).

Tabular values are lightweight concrete and no additional reduction factor is needed. 4

5 No additional reduction factors for spacing or edge distance need to be applied.

6 Comparison of the tabular values to the steel strength is not necessary. Tabular Values control.

Tabular values are for static loads only. For seismic tenison loads, multiply cracked concrete tabular values in tension by $\alpha_{N,seis} = 0.75$. 7

8 For seismic shear, an additional factor must be applied to the cracked concrete tabular values for seismic conditions:

1/4-in diameter by 1-5/8-in nominal embedment depth - $\alpha_{v_{vess}} = 0.44$ 1/4-in diameter by 2-1/2-in nominal embedment depth - $\alpha_{v_{vess}} = 0.85$ See Section 3.1.8 for additional information on seismic applications.

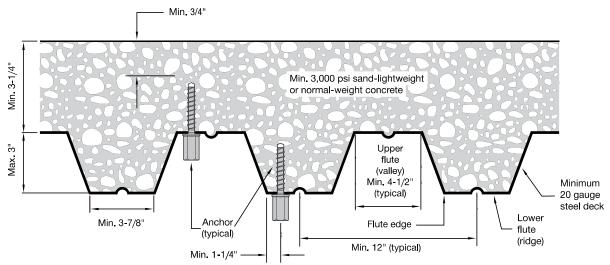


Figure 2 — Installation of Hilti KWIK HUS-EZ I and KWIK HUS-EZ E in soffit of concrete over steel deck floor and roof assemblies

1 Anchors may be placed in the upper or lower flute of the steel deck profile provided the minimum concrete cover above the drilled hole is satisfied. Anchors in the lower flute may be installed with a maximum 1-inch offset in either direction from the center of the flute. The offset distance may be increased proportionally for profiles with lower flute widths greater than those shown provided the minimum lower flute edge distance is also satisfied.

DESIGN INFORMATION IN CONCRETE PER CSA A23.3

Limit State Design of anchors is described in the provisions of CSA A23.3 Annex D for post-installed anchors tested and assessed in accordance with ACI 355.2 for mechanical anchors and ACI 355.4 for adhesive anchors. This section contains the Limit State Design tables with unfactored characteristic loads that are based on the published loads in ICC Evaluation Services ESR-3027. These tables are followed by factored resistance tables. The factored resistance tables have characteristic design loads that are prefactored by the applicable reduction factors for a single anchor with no anchor-to-anchor spacing or edge distance adjustments for the convenience of the user of this document. All the figures in the previous ACI 318 Chapter 17 design section are applicable to Limit State Design and the tables will reference these figures.

For a detailed explanation of the tables developed in accordance with CSA A23.3 Annex D, refer to Section 3.1.8. Technical assistance is available by contacting Hilti Canada at (800) 363-4458 or at www.hilti.com.

Nominal anchor diameter in.	Internal thread diameter (UNC)	Tensile ³ N _{sar} Ib (KN)	Shear ⁴ V _{sar} Ib (kN)	Seismic shear ⁵ V _{sar.eq} Ib (kN)
1/4	1/4-20	3,370	750	335
1/4	1/4-20	(15.0)	(3.3)	(1.5)
1 //	3/8-16	3,370	725	620
1/4	3/0-10	(15.0)	(3.2)	(2.8)
2 /0	1/0.10	5,515	1,040	1,040
3/8	1/2-13	(24.5)	(4.6)	(4.6)

Table 11 — Steel resistance for Hilti KWIK HUS-EZ I and KWIK HUS-EZ E carbon steel screw anchor^{1,2}

1 See Section 3.1.8 of Hilti Product Technical Guide Ed 21 to convert factored resistance value to ASD value.

2 Hilti KWIK HUS-EZ I carbon steel screw anchors are to be considered brittle steel elements.

4 Shear determined by static shear tests with V_{sar} < 0.6 $A_{saV} \phi_s f_{uta} R$ as noted in CSA A23.3 Annex D.

5 Seismic shear values determined by seismic shear tests with V_{stran} ≤ 0.60 A_{set} φ_s f_{uta} R as noted in CSA A23.3 Annex D. See Section 3.1.8 of Hilti Product Technical Guide Ed 21 for additional information on seismic applications.

³ Tensile $N_{sar} = A_{seN} \phi_s f_{uta} R$ as noted in CSA A23.3 Annex D.



Design parameter		Symbol	Units	Nomin	al anchor dia	ameter	Ref
Design parameter		Symbol	Units	1,	/4	3/8	A23.3
Anchor O.D.		d _a	in.		25	0.375	
		u _a	(mm)		.4)	(9.5)	
Effective embedment ²		h _{ef}	in.	1.18	1.92	1.54	
		'ef	(mm)	(30)	(49)	(39)	
Minimum nominal embedment ²		h _{nom}	in.	1-5/8	2-1/2	2 1/8	
		nom	(mm)	(41)	(64)	(54)	
Minimum concrete thickness		h _{min}	in.	3-1/4	4-1/8	3 5/8	
			(mm)	(83) 2.00	(105) 2.78	(92)	
Critical edge distance		C _{ac}	in. (mm)		(71)	(70)	
			(mm) in.	(51)	.5	2.25	
Minimum spacing at critical edge distance		S _{min,cac}	(mm)	(3		(57)	
			in.		5) 50	1.5	
Minimum edge distance		C _{min}	(mm)	(3		(38)	
			in.		.0	3	
Minimum anchor spacing at minimum edge distance		for s >	(mm)	-	6)	(76)	
			in.	2	2-7/8	2 3/8	
Mininimum hole depth in concrete		h _o	(mm)	(51)	(73)	(60)	
			psi	125		106,975	
Minimum specified ultimate strength		f _{uta}	(N/mm ²)		52)	(826)	
			in ²	```)45	0.086	
Effective tensile stress area		A _{se,N}	(mm²)	(29		(55.5)	
Steel embed. material resistance factor for reinforcen	nent	φ _s	-		0.85		8.4.3
Resistance modification factor for tension, steel failur	re modes ³	R	-		0.70		D.5.3
Resistance modification factor for shear, steel failure	modes ³	R	-		0.65		D.5.3
Enders and standard and the second state of the			lb	3,3	370	5,475	D 040
Factored steel resistance in tension		N _{sar}	(kN)	(15	5.0)	(24.4)	D.6.1.2
Eastard staal registered in shear		V	lb	7!	50	NI/A	D.7.1.2
Factored steel resistance in shear	1/4-20 UNC	V _{sar}	(kN)	(3	.3)	N/A	0.7.1.2
Factored steel resistance in shear, seismic	internal thread	V	lb	33	35	N/A	
		V _{sar,eq}	(kN)	(1	.5)	IN/A	
Factored steel resistance in shear		v	lb	72	25	N/A	D.7.1.2
Factored steel resistance in snear	3/8-16 UNC	V _{sar}	(kN)	(3	.2)	N/A	D.7.1.2
Factored steel resistance in shear, seismic	internal thread	v	lb	62	20	N/A	
		V _{sar,eq}	(kN)	(2	.8)	,	
Factored steel resistance in shear		V _{sar}	lb			1040	
	1/2-13 UNC	sar	(kN)	N	/A	(4.6)	
Factored steel resistance in shear, seismic	internal thread	V _{sar,eq}	lb			1040	
			(kN)			(4.6)	
Coeff. for factored conc. breakout resistance, uncrac		k _{c,uncr}	-		10		D.6.2.2
Coeff. for factored conc. breakout resistance, cracke		k _{c.cr}	-		7		D.6.2.2
Modification factor for anchor resistance, tension, un	cracked conc.4	Ψ _{c,N}	-	-	1.0		D.6.2.6
Anchor category		-	-	3	1	1	D.5.3 (c)
Concrete material resistance factor		Ф _с	-		0.65	1	8.4.2
Resistance modification factor for tension and shear, modes, Condition $B^{\scriptscriptstyle 5}$	concrete failure	R	-	0.75	1.00	1.00	D.5.3 (c)
			lb	665	1,645		-
Factored pullout resistance in 20 MPa uncracked cor	ncrete®	N _{pr,uncr}	(kN)	(3.0)	(7.3)	N/A	D.6.3.2
			lb	340	815	.	D C C C
Factored pullout resistance in 20 MPa cracked concr	ete ⁶	N _{pr,cr}	(kN)	(1.5)	(3.6)	N/A	D.6.3.2
			lb	275	815	N1/A	Daac
Factored seismic pullout resistance in 20 MPa cracked	a concrete°	N _{pr,eq}	(kN)	(1.2)	(3.6)	N/A	D.6.3.2

1 Design information in this table is taken from ICC-ES ESR-3027, tables 6, 7, and 8, and converted for use with CSA A23.3 Annex D.

2 3

4

The KWIK HUS-EZ I is considered a brittle steel element as defined by CSA A23.3 Annex D section D.2. For all design cases, $\psi_{e,N} = 1.0$. The appropriate coefficient for breakout resistance for cracked concrete ($k_{e,n}$) or uncracked concrete ($k_{e,n-1}$) must be used. For use with the load combinations of CSA A23.3 chapter 8. Condition B applies where supplementary reinforcement in conformance with CSA A23.3 section D.5.3 is not provided, or where pullout or pryout strength governs. For cases where the presence of supplementary reinforcement can be verified, the resistance modification factors associated with Condition A may be used. 5 may be used.

6 For all design cases, $\psi_{e,P}$ = 1.0. NA (not applicable) denotes that this value does not control for design. See section 4.1.4 of ESR-3027 for additional information.

Tension - N Shear - V f'_ = 25 $f'_{0} = 40$ $f'_{0} = 20$ f'_ = 25 f' = 40 $f'_{0} = 20$ $f'_{0} = 30$ $f'_{0} = 30$ Nominal Strength Concrete Pullout МРа MPa ŇРа МРа МРа МРа МРа ŇРа anchor Effective Nominal Effec-Reduction material Strength (2,900)(3,625 (4,350 (5,800)(2,900)(3,625 (4,350 (5,800 embed. (2500 psi diameter embed. tiveness Factor resistance psi) psi) psi) psi) psi) psi) psi) psi) in. (mm) in. (mm) Factor Tension factor concrete) lb (kN) in. 1.18 1-5/8 1305 665 710 750 820 805 900 985 1,135 10 0.75 0.65 (30) (5.8) (3.0) (3.2)(3.3)(3.6)(3.6)(4.0)(5.1) (41) (4.4)1/4 1.92 2-1/2 2350 1,645 1,840 2,015 2,325 2,225 2,490 2,725 3,145 10 0.65 1 (49) (64) (10.5)(7.3)(8.2)(9.0)(10.3)(9.9)(12.1)(11.1)(14.0)1.54 2-1/8 1,595 1,785 1.955 2,260 1.595 1,785 1,955 2.260 3/8 10 1 0.65 N/A (39) (54) (7.1)(7.9)(8.7) (10.0)(7.1)(7.9)(10.0)(8.7)

Table 13 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E carbon steel screw anchor factored resistance with concrete/pullout failure in uncracked concrete^{1,2,3,4,5}

Table 14 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E carbon steel screw anchor factored resistance with concrete/pullout failure in cracked concrete^{1,2,3,4,5}

								Tensio	on - N _r			Shea	ır - V _r	
							<i>f</i> ' _c = 20	f' _c = 25	<i>f</i> ' _c = 30	<i>f</i> ' _c = 40	<i>f</i> ' _c = 20	f' _c = 25	<i>f</i> ' _c = 30	f' _c = 40
Nominal				Strength	Concrete	Pullout	MPa	MPa	MPa	MPa	MPa	MPa	MPa	MPa
anchor	Effective	Nominal	Effec-	Reduction	material	Strength	(2,900	(3,625	(4,350	(5,800	(2,900	(3,625	(4,350	(5,800
diameter	embed.	embed.	tiveness	Factor	resistance	(2500 psi	psi)	psi)	psi)	psi)	psi)	psi)	psi)	psi)
in.	in. (mm)	in. (mm)	Factor	Tension	factor	concrete)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)	lb (kN)
d _a in (mm)	h _{ef} (mm)	h _{nom} (mm)	k _{cr}	R	Φ _c	N _{p,uncr} (N/mm²)	20	25	30	40	20	25	30	40
	1.18	1-5/8	7	0.75	0.65	665	340	360	385	415	565	630	690	795
1/4	(30)	(41)		0.75	0.05	(3.0)	(1.5)	(1.6)	(1.7)	(1.9)	(2.5)	(2.8)	(3.1)	(3.5)
1/4	1.92	2-1/2	7	1	0.65	1165	815	910	1,000	1,155	1,800	1,740	1,910	2,205
	(49)	(64)			0.05	(5.2)	(3.6)	(4.1)	(4.4)	(5.1)	(8.0)	(7.7)	(8.5)	(9.8)
3/8	1.54	2-1/8	7	1	0.65	N/A	1,120	1,250	1,370	1,580	1,120	1,250	1,370	1,580
5/6	(39)	(54)		I	0.00	in/A	(5.0)	(5.6)	(6.1)	(7.0)	(5.0)	(5.6)	(6.1)	(7.0)

See section 3.1.8 to convert design strength value to ASD value. 1

2 Linear interpolation between embedment depths and concrete compressive strengths is not permitted.

3 Apply spacing, edge distance, and concrete thickness factors in tables 5 to 6 as necessary. Compare to the steel values in table 9.

The lesser of the values is to be used for the design.

Tabular values are for normal weight concrete only. For lightweight concrete multiply design strength by λ_{a} as follows: 4 for sand-lightweight, $\lambda_a = 0.68$; for all-lightweight, $\lambda_a = 0.60$

5 Tabular values are for static loads only. Seismic design is not permitted for uncracked concrete. For seismic tension loads, multiply cracked concrete tabular values in tension by the fol-5 lowing reduction factors:

1/4-in diameter by 1-5/8-in nominal embedment depth - $\alpha_{_{N,seis}}$ = 0.60

1/4-in diameter by 2-1/2-in nominal embedment depth - $\alpha_{N,sels}^{N,sels}$ = 0.75. No reduction needed for seismic shear. See section 3.1.8 for additional information on seismic applications.



Table 15 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E in the soffit of uncracked lightweight concrete over metal deck^{1,2,3,4,5,6,7}

	Nominal internal		Installation in lower flute				Installation in upper flute			
Nominal anchor		Nominal embed. depth in. (mm)	Tension - N _r		Shear - V _r		Tension - N _r		Shear - V _r	
	thread diameter in.		f' _c = 20 MPa (2,900 psi) kN	f' _c = 30 MPa (4,350 psi) kN	f' _c = 20 MPa (2,900 psi) kN	f' _c = 30 MPa (4,350 psi) kN	f' _c = 20 MPa (2,900 psi) kN		f' _c = 20 MPa (2,900 psi) kN	f' _c = 30 MPa (4,350 psi) kN
		1-5/8	585	660			720	810		
1 //	1/4-20 UNC	(41)	(2.6)	(2.9)	475	475	(3.2)	(3.6)	560	560
1/4		2-1/2	1,200	1,470	(2.1)	(2.1)	1,255	1,535	(2.5)	(2.5)
		(64)	(5.3)	(6.5)			(5.6)	(6.8)		
		1-5/8	585	660			720	810		
1/4	3/8-16	(41)	(2.6)	(2.9)	565	565	(3.2)	(3.6)	845	845
1/4	UNC	2-1/2	1,200	1,470	(2.5)	(2.5)	1,255	1,535	(3.8)	(3.8)
		(64)	(5.3)	(6.5)			(5.6)	(6.8)		
2 /0	1/2-13	2-1/8	1,100	1,345	1,315	1,315	1,865	2,280	2,015	2,015
3/8	ÚNC	(54)	(4.9)	(6.0)	(5.8)	(5.8)	(8.3)	(10.1)	(9.0)	(9.0)

Table 16 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E in the soffit of cracked lightweight concrete over metal deck^{1,2,3,4,5,6,7,8}

*

			Installation in lower flute			Installation in upper flute					
Nominal Nominal internal anchor thread diameter in. in.	Nominal	rnal Nominal ead embed. neter depth	Tensio	Tension - N _r		Shear - V _r		Tension - N _r		Shear - V _r	
	thread diameter		f' _c = 20 MPa (2,900 psi) kN	f' _c = 30 MPa (4,350 psi) kN	f' _c = 20 MPa (2,900 psi) kN	f' _c = 30 MPa (4,350 psi) kN	f' _c = 20 MPa (2,900 psi) kN		f' _c = 20 MPa (2,900 psi) kN	f' _c = 30 MPa (4,350 psi) kN	
		1-5/8	300	340			365	415			
1/4	1/4-20 UNC	(41)	(1.3)	(1.5)	475	475	(1.6)	(1.8)	560	560	
1/4		2-1/2	595	730	(2.1)	(2.1)	625	765	(2.5)	(2.5)	
		(64)	(2.6)	(3.2)			(2.8)	(3.4)			
		1-5/8	300	340			365	415			
1/4	3/8-16	(41)	(1.3)	(1.5)	565	565	(1.6)	(1.8)	845	845	
1/4	UNC	2-1/2	595	730	(2.5)	(2.5)	625	765	(3.8)	(3.8)	
		(64)	(2.6)	(3.2)			(2.8)	(3.4)			
2 /0	1/2-13	2-1/8	780	955	1,315	1,315	1,305	1,595	2,015	2,015	
3/8	ÚNC	(54)	(3.5)	(4.2)	(5.8)	(5.8)	(5.8)	(7.1)	(9.0)	(9.0)	

See Section 3.1.8 to convert design strength value to ASD value.

Linear interpolation between embedment depths and concrete compressive strengths is not permitted. 2 3

Tabular value is for one anchor per flute. Minimum spacing along the length of the flute is 6 3/8 inches. Tabular value is for lightweight concrete and no additional reduction factor is needed. 4

No additional reduction factors for spacing or edge distance need to be applied. 5

6 Comparison of the tabular values to the steel strength is not necessary. Tabular values control.

Tabular values are for static loads only. For seismic conditions $\alpha_{v_{statis}} = 0.75$ For seismic shear, an additional factor must be applied to the cracked concrete tabular values for seismic conditions: $\alpha_{v_{statis}} = 0.85$ 8

See Section 3.1.8 for additional information on seismic applications.

ALLOWABLE STRESS DESIGN FOR FM SPRINKLER SYSTEMS

Table 17 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E tested load values for FM approval for automatic sprinkler systems¹

Anchor diamenter in.	Hanger rod size	Nominal embedment in.	FM tension test load lb.	FM maximum pipe diameter in.
	2/0 16 LINO	1-5/8	1 475	
1/4	3/8-16 UNC	2-1/2	1,475	4
3/8	1/2-13 UNC	2-1/8	3,800	8

1 Tested in accordance with FM Approval Standard for Pipe Hanger Components for Automatic Sprinklers Systems Class Numbers 1951, 1952 and 1953.

³⁷⁴ Anchor Fastening Technical Guide Edition 21 | 3.0 ANCHORING SYSTEMS | 3.3.8 KWIK HUS-EZ I AND KWIK HUS-EZ E CARBON STEEL SCREW ANCHOR Hilti, Inc. 1-800-879-8000 | en español 1-800-879-5000 | www.hilti.com | Hilti (Canada) Corporation | www.hilti.ca | 1-800-363-4458

DESIGN INFORMATION IN HOLLOW CORE CONCRETE PER ALLOWABLE STRESS DESIGN

Table 18 — Hilti KWIK HUS-EZ I and KWIK HUS-EZ E load values for installations into hollow core concrete panels^{1,2}

		Min. effective	Min.effective base	Allowab	le load ³	Ultimate load	
Hanger rod size	anchor diameter in.	embedment h _{ef} in.	material thickness t in.	Tension lb	Shear Ib ^{4,5}	Tension lb	Shear Ib ^{4,5}
1/4-20 UNC	1/4	1.0/0	1.0/0	455	485	1,810	1,930
3/8-16 UNC	1/4	1-3/8	1-3/8	455	755	1,810	3,025
1/2-13 UNC	3/8	1-1/8	1-1/8	435	N/A	1,750	N/A

1 The admissible anchor location must be established to prevent damage to the prestressed cable during the drilling process. Verify the location and height of the cable with the hollow core plank supplier to confirm admissible anchor location.

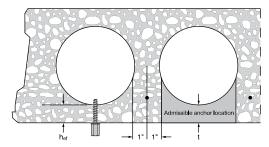
2 Minimum compressive strength of prestressed concrete is 7,000 psi. Published ultimate loads represent the average results conducted in local base materials. Due to variations in materials and dimensionl configurations, on-site testing is required to determine the actual performance.

3 Allowable loads calculated with a factor of safety of 4

4 The bottom of the shear plane adjacent to the top of the coupler.

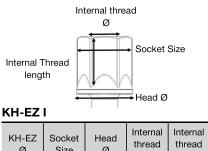
5 Shear values controlled by the steel strength of the screws used to fasten the shear fixture to the KH EZ-I Screw Anchor. The minimum tensile strength of the screw was 125 ksi. Shear design values should consider the screw or threaded rod steel strength.

Figure 3 - Installation of Hilti KWIK HUS-EZ I and KH-EZ E in hollow core concrete



INSTALLATION INSTRUCTIONS

Installation Instructions For Use (IFU) are included with each product package. They can also be viewed or downloaded online at www.hilti.com. Because of the possibility of changes, always verify that downloaded IFU are current when used. Proper installation is critical to achieve full performance. Training is available on request. Contact Hilti Technical Services for applications and conditions not addressed in the IFU.



ø	Size	Ø	thread Ø	thread length
1/4''	3/8''	0.59''	1/4"	0.37"
1/4''	1/2"	0.65"	3/8''	0.45"
3/8''	11/16"	0.81"	1/2''	0.46"

External thread Ø

External thread length											
KH-EZ	Socket Size Head Ø KH-EZ E										
KH-EZ ØSocket SizeMin Socket HeightHead Head ØInternal 											
1/4''	1/2"	1-1/2"	0.65"	3/8''	1.08"	1.32"					

ORDERING INFORMATION¹

	Internal thread	Internal thread	Drill bit	Minimum	
Description	diameter	length	diameter	embedment	Qty / box
KWIK HUS-EZ 1/4x1-5/8 1/4	1/4	3/8	1/4	1-5/8	100
KWIK HUS-EZ 1/4x2-1/2 1/4	1/4	3/8	1/4	2-1/2	100
KWIK HUS-EZ 1/4x1-5/8 3/8	3/8	7/16	1/4	1-5/8	100
KWIK HUS-EZ 1/4x2-1/2 3/8	3/8	7/16	1/4	2-1/2	100
KWIK HUS-EZ 3/8x2-1/8 1/2	1/2	1/2	3/8	2-1/8	100
KWIK HUS-EZ 1/4x1-5/8 E 3/8	3/8	1	1/4	1-5/8	100

1 All dimensions in inches.

Anchor Fastening Technical Guide Edition 21 | 3.0 ANCHORING SYSTEMS | 3.3.8 KWIK HUS-EZ I AND KWIK HUS-EZ E CARBON STEEL SCREW ANCHOR Hilti, Inc. 1-800-879-8000 | en español 1-800-879-5000 | www.hilti.com | Hilti (Canada) Corporation | www.hilti.ca | 1-800-363-4458

3.3.8